

***vKalc* Calculation Editor** **Examples (v1.0)**

Dark Valley Software

Calculation Examples

The following pages will demonstrate the capabilities of *vKalc* through a series of short and varied calculations.

The final calculation is much more detailed and demonstrates the complete design of a reinforced concrete beam.

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Compound Interest Calculation

Principal sum;	$P_i = 15000\$$
Annual percentage rate (APR);	$r = 4.875\%$
Compound monthly;	$n = 12$; times per year
Full term;	$t_m = 7.5$; years
Total amount accrued over term;	$A_{tm} = P_i \times (1 + r / n)^{(n \times tm)} = 21605\$$
Total interest accrued over term;	$I_{tm} = A_{tm} - P_i = 6605\$$

Day Trading Calculation

Trading account fund;	$P_0 = 40000\$$
Maximum risk on this trade;	risk = 1%
Available funds for this trade;	$P_t = P_0 \times \text{risk} = 400\$$
Current stock price;	$sp_{buy} = 15\$$
Target sale price;	$sp_{sell} = 19\$$
Potential win per share;	$\text{win} = sp_{sell} - sp_{buy} = 4\$$
For a 2:1 win:loss risk;	$\text{loss} = \text{win} / 2 = 2\$$
Set stop loss;	$sp_{stop} = sp_{buy} - \text{loss} = 13\$$
Max share size can trade;	$P_t / \text{loss} = 200$;shares

Terminal Velocity Calculation

Mass of a tennis ball;	$m_{\text{ball}} = 58\text{g}$
Diameter of a tennis ball;	$D_{\text{ball}} = 6.70\text{cm}$
Projected cross-sectional area;	$A_{\text{ball}} = \pi D_{\text{ball}}^2 / 4 = 35.3\text{cm}^2$
Drag coefficient (sphere);	$C_{\text{drag}} = 0.47$
Density of air;	$\rho_f = 1.204\text{kg/m}^3$
Terminal velocity;	$v_T = \sqrt{(2 \times m_{\text{ball}} \times g_o / (C_{\text{drag}} \times \rho_f \times A_{\text{ball}}))} = 23.9\text{m/s}$

Projectile Motion Calculation

Angle of cannon;	$\theta = 30^\circ$
Initial velocity;	$V_i = 150\text{m/s}$
Initial horizontal velocity;	$V_{ix} = V_i \times \cos(\theta) = 130\text{m/s}$
Initial vertical velocity;	$V_{iy} = V_i \times \sin(\theta) = 75\text{m/s}$
Time to reach maximum height;	$t_{\text{max}} = V_{iy} / g_o = 7.65\text{s}$
Maximum height reached;	$h_{\text{max}} = V_{iy} \times t_{\text{max}} - (0.5 \times g_o \times t_{\text{max}}^2) = 287\text{m}$
Total time in the air;	$t_{\text{total}} = 2 \times t_{\text{max}} = 15.3\text{s}$
Range of cannon ball;	$R_{\text{ball}} = V_{ix} \times t_{\text{total}} = 1987\text{m}$

Length of a Clock Pendulum Calculation

For period;

$$T_p = 2.0s$$

Pendulum length required;

$$L = T_p^2 \times g_o / 4\pi^2 = 994\text{mm}$$

Roundabout Calculation

Speed of roundbout;

$$v_{\max} = 3.0\text{m/s}$$

Mass of child;

$$m_{\text{ch}} = 26\text{kg}$$

Distance of child from center;

$$r_{\text{ch}} = 3\text{m}$$

Centripetal acceleration;

$$a_{\text{cp}} = v_{\max}^2 / r_{\text{ch}} = 3\text{m/s}^2$$

Centripetal force;

$$F_{\text{cp}} = m_{\text{ch}} \times a_{\text{cp}} = 78\text{N}$$

Weight of child;

$$F_{\text{ch}} = m_{\text{ch}} \times g_o = 255\text{N}$$

Ratio;

$$F_{\text{cp}} / F_{\text{ch}} = 30.6\%$$

Simple pH Calculations*For a weak acid*

Hydrogen ion concentration;

$$H^+ = 1.4e-5;mol$$

(Note, the semicolon placed between the number and the unit, as the unit is not needed for the subsequent calculation)

$$pH = -\log(H^+) = \underline{4.85}$$

For a concentrated acid

Hydrogen ion concentration;

$$H^+ = 0.035mol$$

$$pH = -\log(H^+ \times mol^{(-1)}) = \underline{1.46}$$

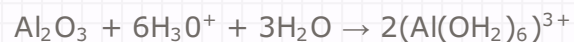
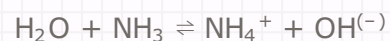
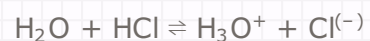
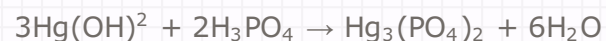
Check in reverse from a pH value

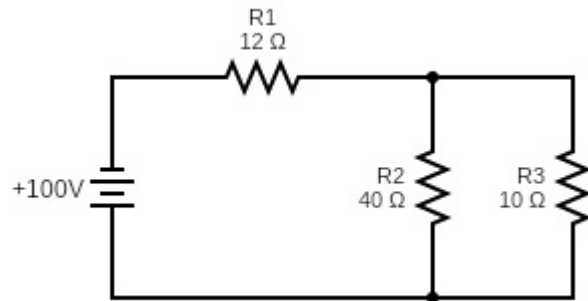
pH value of liquid;

$$pH = 8.48$$

Hydrogen ion concentration;

$$H^+ = 10^{(-pH)} = \underline{3.31e-09}$$

*(Note, the solver will ignore superscripts ending in '+' or '-')***Chemical Equation Notation**

Electric Circuit Calculation

Source voltage;

$$V_s = 100V$$

Resistor;

$$R_1 = 12\Omega$$

$$R_2 = 40\Omega$$

$$R_3 = 10\Omega$$

For resistors connected in parallel;

$$R_{eq} = (1 / R_2 + 1 / R_3)^{(-1)} = 8\Omega$$

Total circuit resistance;

$$R_T = R_1 + R_{eq} = 20\Omega$$

Total circuit current;

$$I_T = V_s / R_T = 5A$$

Voltage drop across R_1 ;

$$V_{R1} = I_T \times R_1 = 60V$$

Voltage drop across R_2 and R_3 ;

$$V_p = V_s - V_{R1} = 40V$$

Current passing through R_2 ;

$$I_{R2} = V_p / R_2 = 1A$$

Current passing through R_3 ;

$$I_{R3} = I_T - I_{R2} = 4A$$

Electric Circuit Calculation (cont'd...)Voltage drop across R_2 ;

$$V_{R2} = I_{R2} \times R_2 = \underline{40V}$$

Voltage drop across R_3 ;

$$V_{R3} = I_{R3} \times R_3 = \underline{40V}$$

Total power consumed;

$$P_T = V_s \times I_T = \underline{500W}$$

Power dissipated by resistor;

$$P_{R1} = V_{R1} \times I_T = \underline{300W}$$

$$P_{R2} = V_{R2} \times I_{R2} = \underline{40W}$$

$$P_{R3} = V_{R3} \times I_{R3} = \underline{160W}$$

Electromagnetic Force Calculation

Magnetic constant;

$$\mu_0 = 4\pi \times 10^{(-7)}\text{H/m}$$

Electric current through solenoid;

$$I_{sol} = 1.5A$$

Number of turns on solenoid;

$$N_{sol} = 550;\text{turns}$$

Diameter of solenoid;

$$D_{sol} = 16\text{mm}$$

Area of solenoid;

$$A_{sol} = \pi D_{sol}^2 / 4 = \underline{201}\text{mm}^2$$

Diameter of armature;

$$D_{arm} = 12\text{mm}$$

Gap between solenoid and armature;

$$g_{ap} = (D_{sol} - D_{arm}) / 2 = \underline{2}\text{mm}$$

Electromagnetic force (on armature);

$$F_{arm} = (N_{sol} \times I_{sol})^2 \times \mu_0 \times A_{sol} / 2g_{ap}^2 = \underline{21.5N}$$

Reinforced Concrete Beam Design**Material details**

Density of concrete;

$$\gamma_c = 25 \text{ kN/m}^3$$

Characteristic strength of concrete;

$$f'_c = 40 \text{ N/mm}^2; \text{ (30MPa minimum)}$$

$$f'_{c_sqrt} = \sqrt{f'_c} \times \sqrt{(\text{N/mm}^2)} = 6.32 \text{ N/mm}^2$$

Elastic modulus;

$$E_c = ((2500 \text{ kg/m}^3) / (\text{kg/m}^3))^{1.5} \times 0.043 \times f'_{c_sqrt}$$

$$E_c := 34 \text{ kN/mm}^2$$

Characteristic strength of reinf;

$$f_y = 420 \text{ N/mm}^2$$

Elastic modulus;

$$E_s = 200 \text{ kN/mm}^2$$

Modular ratio;

$$\eta = E_s / E_c = 5.88$$

Cover to rebar;

$$c_{min} = 40 \text{ mm}$$

Beam section details

Depth of beam;

$$h = 600 \text{ mm}$$

Width of beam;

$$b = 300 \text{ mm}$$

Span of beam;

$$L = 5000 \text{ mm}$$

Minimum depth as per ACI;

$$h_{min} = L / 16 = 312 \text{ mm}$$

Dead load of beam;

$$DL_{beam} = h \times b \times \gamma_c = 4.5 \text{ kN/m}$$

$$DL_{beam_f} = 1.2 \times h \times b \times \gamma_c = 5.4 \text{ kN/m}$$

Reinforced Concrete Beam Design (cont'd...)**Floor Loads**

Floor loads;

$$DL_{\text{slab}} = 2.45 \text{ kN/m}^2$$

$$DL_{\text{screed}} = 1.75 \text{ kN/m}^2$$

$$DL_{\text{finishes}} = 0.6 \text{ kN/m}^2$$

$$DL_{\text{services}} = 0.3 \text{ kN/m}^2; \quad (\text{includes ceilings})$$

$$DL_{\text{partitions}} = 3.0 \text{ kN/m}^2$$

Total dead load on floor;

$$DL_{\text{floor}} = \text{sum}(DL_{\text{slab}}, DL_{\text{screed}}, DL_{\text{finishes}}, DL_{\text{services}}, DL_{\text{partitions}})$$

$$DL_{\text{floor}} := 8.1 \text{ kN/m}^2$$

Total live load on floor;

$$LL_{\text{floor}} = 1.5 \text{ kN/m}^2$$

Total loading on 150mm floor;

$$UDL_{\text{floor}} = DL_{\text{floor}} + LL_{\text{floor}} = 9.6 \text{ kN/m}^2$$

$$UDL_{\text{floor}_f} = 1.2 \times DL_{\text{floor}} + 1.6 \times LL_{\text{floor}} = 12.1 \text{ kN/m}^2$$

From Analysis

Loaded width of beam;

$$b_L = 5000 \text{ mm}$$

Ultimate design moment;

$$M_u = (DL_{\text{beam}_f} + b_L \times UDL_{\text{floor}_f}) \times L^2 / 8 = 206 \text{ kNm}$$

Ultimate design shear;

$$V_u = (DL_{\text{beam}_f} + b_L \times UDL_{\text{floor}_f}) \times L / 2 = 165 \text{ kN}$$

Reinforced Concrete Beam Design (cont'd...)**Check Bending**

Design moment;

$$M_u := 206 \text{ kNm}$$

Area of steel provided;

$$A_s = 4T25 = 1963 \text{ mm}^2$$

$$\Phi_{\text{main}} = 25 \text{ mm}; \Phi_{\text{link}} = 10 \text{ mm}$$

Depth to tension steel;

$$d = h - c_{\text{min}} - \Phi_{\text{link}} - \Phi_{\text{main}} / 2 = 538 \text{ mm}$$

Min area of steel;

$$A_{s_min} = \max(b \times d \times f'_{c_sqrt} / 4f_y, 1.4 \text{ N/mm}^2 \times b \times d / f_y)$$

$$A_{s_min} := 607 \text{ mm}^2$$

Steel ratio;

$$\rho = A_s / (b \times d) = 0.0122$$

Depth of compression block;

$$a = \rho \times f_y \times d / (0.85 \times f'_c) = 80.8 \text{ mm}$$

Ratio;

$$\beta_1 = \max(0.65, 0.85 - (0.05 \times (f'_c - 30 \text{ N/mm}^2) / 7 \text{ N/mm}^2)) = 0.779$$

Depth to neutral axis;

$$c = a / \beta_1 = 104 \text{ mm}$$

Net tensile strain;

$$\epsilon_t = 0.003 \times (d - c) / c = 0.0125$$

Net tensile strain in tension controlled zone

Strength reduction factor;

$$\Phi = \min(\max(0.65 + (\epsilon_t - 0.002) \times (250 / 3), 0.65), 0.9) = 0.9$$

Nominal bending capacity;

$$M_n = A_s \times f_y \times (d - a / 2) = 410 \text{ kNm}$$

Permissible bending capacity;

$$\Phi M_n = \Phi \times M_n = 369 \text{ kNm}$$

$$\text{if}(\Phi M_n < M_u, \text{Bending} = \text{"Fail"}, \text{Bending} = \text{"Pass"})$$

$$\text{Bending} := \text{Pass}$$

Reinforced Concrete Beam Design (cont'd...)**Check Shear**

Design shear force; $V_u := 165\text{kN}$

For normal weight concrete; $\lambda = 1.0$

Shear reduction factor; $\Phi = 0.75$

Nominal concrete shear strength; $V_c = 0.17 \times \lambda \times f'_{c_sqrt} \times b \times d = 173\text{kN}$

Nominal rebar shear strength; $V_s = \max((V_u - (\Phi \times V_c)) / \Phi, 0\text{kN}) = 46.6\text{kN}$

Max allowable rebar shear strength; $V_{s_max} = 4 \times V_c = 693\text{kN}$

Where V_s exceeds $2V_c$ reduce the maximum link spacing by one-half

$$V_{s_limit} = 2 \times V_c = 347\text{kN}$$

Max link spacing; $s_{v_max} = 1.0 \times \min(d / 2, 600\text{mm}) = 269\text{mm}$

Try spacing; $s_v = 200\text{mm}$

Min area of shear steel required; $A_{sv_min} = \max(0.062 \times f'_{c_sqrt}, 0.35\text{N/mm}^2) \times b / f_y = 280\text{mm}^2/\text{m}$

Area of shear steel required; $A_{sv_reqd} = \max(V_s / (f_y \times d), A_{sv_min}) = 280\text{mm}^2/\text{m}$

Area of shear steel provided; $A_{sv_prov} = 2\text{T}10@200\text{mm} = 785\text{mm}^2/\text{m}$

if($A_{sv_reqd} > A_{sv_prov}$, Shear = "Fail", Shear = "Pass")

Shear := Pass

Reinforced Concrete Beam Design (cont'd...)**Check Deflection**

Area of tension reinforcement;	$A_{s_tens} = A_s = 1963 \text{mm}^2$
Tension reinforcement ratio;	$\rho := 0.0122$
Depth to compression steel;	$d' = 60 \text{mm}$
Area of compression reinforcement;	$A_{s_comp} = 0 \text{mm}^2$
Compression reinforcement ratio;	$\rho' = A_{s_comp} / (b \times d) = 0$
Moment of inertia (gross);	$I_g = b \times h^3 / 12 = 540000 \text{cm}^4$
	$y_t = h / 2 = 300 \text{mm}$
For normal weight concrete;	$\lambda = 1.0$
Modulus of rupture;	$f_r = 0.62 \times \lambda \times f'_{c_sqrt} = 3.92 \text{N/mm}^2$
Cracking moment;	$M_{cr} = f_r \times I_g / y_t = 70.6 \text{kNm}$
Neutral axis depth factor;	$x_{na} = -\eta \times (\rho + \rho') + \sqrt{(\eta^2 \times (\rho + \rho')^2 + 2 \times \eta \times (\rho + d' \times \rho' / d))}$
	$x_{na} := 0.314$
Moment of inertia (cracked);	$I_{cr} = (x_{na}^3 / 3 + \eta \times \rho \times (1 - x_{na})^2 + \eta \times \rho' \times (x_{na} - d' / d)^2) \times b \times d^3$
	$I_{cr} := 205132 \text{cm}^4$
Service dead load moment;	$M_D = (DL_{beam} + b_L \times DL_{floor}) \times L^2 / 8 = 141 \text{kNm}$
Service live load moment;	$M_L = (b_L \times LL_{floor}) \times L^2 / 8 = 23.4 \text{kNm}$

Reinforced Concrete Beam Design (cont'd...)**Instantaneous deflections**

Moment factor;

$$f_m = M_{cr} / M_D = 0.502$$

Moment of inertia (effective);

$$\text{if}(f_m > 1, I_e = I_g, I_e = f_m^3 \times I_g + (1 - f_m^3) \times I_{cr})$$

$$I_e := 247474 \text{ cm}^4$$

Deflection due to dead load;

$$\delta_{dead} = 5 \times L^2 \times M_D / (48 \times E_c \times I_e) = 4.35 \text{ mm}$$

Moment factor;

$$f_m = M_{cr} / (M_D + M_L) = 0.43$$

Moment of inertia (effective);

$$\text{if}(f_m > 1, I_e = I_g, I_e = f_m^3 \times I_g + (1 - f_m^3) \times I_{cr})$$

$$I_e := 231796 \text{ cm}^4$$

Deflection due to dead plus live;

$$\delta_{total} = 5 \times L^2 \times (M_D + M_L) / (48 \times E_c \times I_e) = 5.42 \text{ mm}$$

Movement after installation;

$$\delta_{install} = \delta_{total} - \delta_{dead} = 1.07 \text{ mm}$$

Movement after installation limit;

$$\delta_{limit} = L / 480 = 10.4 \text{ mm}$$

$$\text{if}(\delta_{limit} < \delta_{install}, \text{Deflection} = \text{"Fail"}, \text{Deflection} = \text{"Pass"})$$

$$\text{Deflection} := \text{Pass}$$

Reinforced Concrete Beam Design (cont'd...)**Long term deflections**

Moment factor;

$$f_m = M_{cr} / (M_D + 0.25 \times M_L) = \underline{0.482}$$

Moment of inertia (effective);

$$\text{if}(f_m > 1, I_e = I_g, I_e = f_m^3 \times I_g + (1 - f_m^3) \times I_{cr})$$

$$I_e := \underline{242593} \text{cm}^4$$

Defl'n due to dead plus sust live;

$$\delta_{sust} = 5 \times L^2 \times (M_D + 0.25 \times M_L) / (48 \times E_c \times I_e) = \underline{4.63} \text{mm}$$

Load duration coefficients;

$$\xi_{5\text{years}} = 2.0$$

$$\xi_{12\text{months}} = 1.4$$

$$\xi_{6\text{months}} = 1.2$$

$$\xi_{3\text{months}} = 1.0$$

Time dependant multipliers;

$$\lambda_{5\text{years}} = \xi_{5\text{years}} / (1 + 50 \times \rho') = \underline{2}$$

$$\lambda_{12\text{months}} = \xi_{12\text{months}} / (1 + 50 \times \rho') = \underline{1.4}$$

$$\lambda_{6\text{months}} = \xi_{6\text{months}} / (1 + 50 \times \rho') = \underline{1.2}$$

$$\lambda_{3\text{months}} = \xi_{3\text{months}} / (1 + 50 \times \rho') = \underline{1}$$

Long term movement;

$$\delta_{LT} = \delta_{install} + (\lambda_{5\text{years}} \times \delta_{sust}) = \underline{10.3} \text{mm}$$

Movement after install limit;

$$\delta_{limit} = L / 480 = \underline{10.4} \text{mm}$$

$$\text{if}(\delta_{limit} < \delta_{LT}, \text{Deflection} = \text{"Fail"}, \text{Deflection} = \text{"Pass"})$$

$$\text{Deflection} := \underline{\text{Pass}}$$